

Ministry of Higher Education and Scientific Research
DJILLALI LIABES University, Sidi Bel Abbas
Faculty of Technology



**Polycopy « Physicochemical and
biological treatment of wastewater»**
(Practical work)

Writtenby:

Dr. DRA Rafik El Arslene (Maitre de conférences –B)

Foreword

The objectives of this handbook are to introduce students in the Master's program in Environmental Process Engineering and Process Engineering to the theoretical knowledge acquired in the Physicochemical and Biological Treatment of Wastewater course (wastewater purification).

Students will be able to use bench-top measuring equipment, as well as pilots and software, to carry out water purification studies.

The content of this module enables students to understand the fundamentals of biological wastewater treatment, and to design the various wastewater treatment plants intended for urban or industrial settings.

Contents :

1st TP group: Wastewater characterization

- TP01: Chemical Oxygen Demand (COD).
- TP02: Biochemical oxygen demand (BOD5).
- TP03: Suspended solids (SS), and water oxidizability index (IP).

2nd TP group: Physico-chemical treatment

- TP04: Coagulation and flocculation
- TP05: Settling-Part 1 (Kynch's Law)
- TP06: Settling - part 2 (MOHLMAN Index and Sludge Index)

3rd TP group: tertiary treatment

- TP07: Disinfection of treated water (break-point)

SUMMARY

Foreword

TP01: Chemical Oxygen Demand (COD)	01
TP02: Biochemical oxygen demand (BOD ₅)	05
TP03: Suspended solids (SS), and water oxidizability index (IP)	09
TP04: Coagulation and flocculation	14
TP05: Settling-Part1 (KYNCH's Law)	18
TP06: Settling-Part2 (MOHLMAN Index and Sludge Index)	24
TP07: Disinfection of treated water (break-point)	29

References

TP01 :
DETERMINATION OF CHEMICAL OXYGEN
DEMAND (COD)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 01 :
DETERMINATION OF CHEMICAL OXYGEN DEMAND
(COD)
Standard NF T90-101 (0-1000mgO₂/L)

- INTRODUCTION :

As they break down, organic matter consumes the oxygen dissolved in water. If too abundant, they can cause excessive oxygen consumption, resulting in asphyxiation of aquatic organisms. Chemical oxygen demand (COD) is a measure of the concentration of organic or mineral matter, dissolved or suspended in water, in terms of the quantity of oxygen required for its total chemical oxidation. By measuring COD, we can assess the organic matter load of wastewater before and after physical, chemical or biological treatment, in order to monitor the operation of a WWTP and the activity of micro-organisms, making it an indicator of the degree of pollution.

Chemical Oxygen Demand (COD): is the mass concentration, expressed in mg/L, of oxygen (O₂), equivalent to the quantity of potassium dichromate (K₂Cr₂O₇) consumed by the oxidizable matter in the solution.

- PRINCIPLE:

- COD determination comprises 02 steps:
 - ✓ Stage 1: chemical oxidation of the reducing organic matter contained in the water, by an excess of potassium dichromate K₂Cr₂O₇. This is a so-called indirect determination.
- This oxidation is carried out in a sulfuric medium, in the presence of Ag₂SO₄ and HgSO₄, boiling at reflux (gentle) for 1.5 hours in a flask fitted with a cooler.
 - ✓ Step 2: After cooling, measure excess K₂Cr₂O₇ with MOHR salt.

- PURPOSE:

- Determine the Chemical Oxygen Demand (COD in mg/L) of a water sample.

- MATERIALS, MEASURING EQUIPMENT AND PRODUCTS :

Measuring equipment	Products
<ul style="list-style-type: none"> - Graduated burette - Graduated pipette + pro-pipette - 100ml, 250ml volumetric flasks. - 250 ml beaker. - Stirrer + magnetic bar. - Thermometer or electro-metric probe. 	<ul style="list-style-type: none"> - Sample water - Potassium dichromate (K₂Cr₂O₇ at 0.04M) M=294 g/mol - MOHR salt [(NH₄)₂Fe(SO₄)₂ · 6H₂O] at C₂ concentration (approx. 0.12M) M=392g/mol - Mercury sulfate (HgSO₄) - Silver sulfate (Ag₂SO₄) at 10g/L - H₂SO₄ at C=4M.
<p>➤ <u>Arrangement of a reflux heating system :</u></p>	

<ul style="list-style-type: none"> - Flat-bottomed ground-glass flask (150 or 250ml) + stopper. - Ball or serpentine refrigerant - Flexible hoses for water inlet and outlet - Balloon heater - Elevating support. - Stand for suspending flask and coolant 	<ul style="list-style-type: none"> - Pumice stones or boiling regulator beads - Ferroin (ferrous orthophenanthroline - color indicator) - Ice bath - Distilled water.
---	---

- HANDLING (Operating mode) :

Before taking the test sample, the water sample must be carefully homogenized by shaking the bottle, and if the water sample has been taken from the inlet of a wastewater treatment plant, it is preferable to dilute it 2 to 5 times (to avoid the risk that the dose of $K_2Cr_2O_7$ introduced into the water to be analyzed is too low, and that it is entirely reduced by the sample, and without an excess of $K_2Cr_2O_7$ at the end of the reaction, the measurement is impossible).

➤ **Stage 1: oxidation of organic matter in water.**

- Dans un ballon à fond plat muni d'un bouchon, introduire :
- $V_0 = 10\text{ml}$ précisément d'eau à analyser (effluent).
- 5ml de $K_2Cr_2O_7$ à $C_1 = 0.04\text{M}$ contenant 0.4g de $HgSO_4$.
- **Ajouter 05 à 06 billes régulatrice d'ébullition (ou pierre ponce), boucher et homogénéiser en agitant doucement.**

1- Using a pipette, slowly and carefully add 15ml ($H_2SO_4(4\text{M}) + Ag_2SO_4(10\text{g/L})$) in a fume hood. Shake the flask circularly and cool in an ice bath.

2- Place the flask in its heating support (flask heater).

3- Place the cooler (ball or coil) on top of the flask and supply it with tap water.

4- Start heating at gentle boiling for $1\text{h}:30$.

Réaliser part-3 during heating.

5- After $1\text{h}:30$, switch off the heater.

6- Allow to cool for a few minutes, then wash the inside wall of the cooler with distilled water, carefully pouring about 75ml of distilled water through the top of the cooler.

7- Remove the flask from the heater and cooler, then cap the flask.

8- Transfer the contents of the flask to a 250ml Erlenmeyer flask, rinsing the flask with a minimum of distilled water and adding the wash water to the mixture.

9- Now proceed to step 2.

➔ **NB : performing a blank test (in parallel)**

- Follow the same steps as in step-1, except use 10ml (V_0) of distilled water instead of the water sample (effluent).

✓ **Step 2: Dose excess oxidant with MOHR salt (Reducer).**

➔ **NB : This step applies to both the sample to be analyzed and the blank test.**

- Introduce into the Erlenmeyer flask recovered from step 1:

- A few drops of ferroin (colored indicator for redox assays).

- Introduce the magnetic rod

1- Fill the burette with MOHR salt solution at C_2 (assayed in step-3).

2- Start the colorimetric determination of the excess oxidizing agent ($K_2Cr_2O_7, C_1$) with the reducing MOHR salt solution, pouring drop by drop until the color changes (bleu \square rouge).

3- Note the volume at equivalence (color change) V_e and V_B (equivalent volume to measure organic matter in the blank test).

✓ **Step3: Calibration of MOHR salt reducing solution.**

As this solution (MOHR salt) is unstable over time, its molar concentration needs to be checked regularly, using an acidified ($K_2Cr_2O_7, C_1$) solution.

1- Introduce into an Erlenmeyer flask or beaker :

- $V_{ox} = 10\text{ml}$ of a solution of $K_2Cr_2O_7$ at $C_{ox} = C_1 = 0.04\text{M}$.

- In the fume hood, using a pipette, slowly and carefully add 15ml ($V_{H_2SO_4}$) of H_2SO_4 (4M), shaking the Erlenmeyer circularly and cooling it in an ice bath.

- Add a few drops of indicator solution (ferroïne).

- Attach a magnetic stirring bar and switch on the magnetic stirrer.

2- Fill burette with MOHR salt reducing solution.

3- Dose this reducing solution at C_2 .

4- Note the equivalence volume V_2 responsible for the color change from green-bleu to brown.

5- Calculate the C_2 concentration value by applying the following expression:

$$C_2 \text{ (en M)} = [Fe^{2+}] = 6C_{ox} \cdot V_{ox}/V_2$$

- **QUESTIONS :**

I) Dosing operation (steps 1 and 2).

1- Write the $\frac{1}{2}$ Redox equations relating to each reagent.

The following couples are given: $Cr_2O_7^{2-}/Cr^{3+}$; Fe^{2+}/Fe^{3+} .

2- Deduce the balance reaction (reaction -1) of the colorimetric assay.

3- Complete the following progress table and determine the following expression between

the 02 reagents:
$$n_{ox} = \frac{C_2 \cdot V_e}{6}$$

States	Progress	$.....Cr_2O_7^{2-} + Fe^{2+} +H^+ \rightarrow 2Cr^{3+} +Fe^{3+} +H_2O$					
S. initial	$x=0$	n_{ox} in excess in the balloon	n_{red} to achieve equivalence	excess	0	0	excess
S. Final (Equivalence)	$x_f = x_{eq}$	$n_{(ox)}^f = \dots\dots\dots$	$n_{(red)}^f = \dots\dots\dots$	excess	$2 x_{eq}$	$6 x_{eq}$	excess

4- The total quantity of dichromate ions n_T introduced into the flask before heating was put into excess: a certain quantity of these ions (noted n_{MO}) reacted by oxidizing the organic matter, the other part, the excess ($n_{ox} = n_{excess}$) was dosed by the MOHR salt solution.

- With the help of the diagram given in the PRINCIPLE of the practical work, and knowing that

$n_T = n_{MO} + n_{ox}$, retrouver la relation suivante :
$$n_{MO} = C_1 \cdot V_1 - \frac{C_2 \cdot V_e}{6}$$

- **II) Oxidation of organic matter (OM) and oxygen equivalence :**

The dichromate ions noted n_{MO} , which will enable the oxidation of organic matter, will first react with water H_2O to form oxygen O_2 .

1- Write the $\frac{1}{2}$ Redox equations for the pairs to which the water and dichromate ions belong. Data: $Cr_2O_7^{2-}/Cr^{3+}$; O_2/H_2O .

2- Determine the balance reaction (reaction -2).

It is assumed that the O_2 formed in the previous reaction will subsequently oxidize the organic matter in the water, enabling the COD to be determined.

3- According to reaction-2, we have: **1 mol ion $Cr_2O_7^{2-} \rightarrow 3/2$ moles of O_2 formed.**

- Finding the relationship for n_{MO} and n_{O_2} .

- **III) Determination of « DCO »:**

1- From the previous results in parts I) and II), show the following literal expression :

$$n_{O_2} = \frac{3}{2} \cdot (C_1 \cdot V_1 - \frac{C_2 \cdot V_e}{6})$$

Determine the expression for the effective molar concentration (**in mol/L**) $[O_2]$, then the mass concentration $t_{m(O_2)}$ (**g/L**) in equivalent oxygen, for a volume of water sample V_0 analyzed.

NB : In order to take into account the blank test, it is necessary to make the following correction

before calculation: $V_1 = \frac{V_B \cdot C_2}{6 \cdot C_1}$ avec $C_1 = [Cr_2O_7^{-2}] = 0.04M$

2- Show the following literal expression for COD (mg O₂/L):

$$DCO(mgd' O_2 / L) = \frac{8000 \cdot C_2 (V_B - V_e)}{V_0}$$

3- Calculate the COD value of the water sample analyzed.

4- Knowing that **the standard sets the COD limit at 120mg/L**, for water discharged by the farm after treatment.

- Are the results in line with the standard?

Water quality is classified according to the following quantitative criteria:

0.5 < DCO < 5 mg/L	drinking water
8 < DCO < 100 mg/L	purified water (non-potable)
800 < DCO < 1200 mg/L	domestic wastewater
1500 < DCO < 10000 mg/L	industrial wastewater

- From the table above: deduce the quality of your analyzed water sample.

TP02 :
DETERMINATION OF BIOCHEMICAL
OXYGEN DEMAND (BOD₅)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 02 :
DETERMINATION OF BIOCHEMICAL OXYGEN
DEMAND (BOD₅)

- INTRODUCTION :

BOD, or Biochemical Oxygen Demand, corresponds to the quantity of oxygen required by aerobic micro-organisms in water to oxidize organic matter dissolved or suspended in the water. It therefore represents the potential consumption of oxygen by biological means. This parameter is a good indicator of a water's biodegradable organic matter content (any polluting biodegradable organic matter leads to oxygen consumption) during self-purification processes.

BOD is used to measure the quality of water in a jar (surface water: rivers, lakes..., wastewater: treatment plants, industrial effluents...). The water analyzed contains a quantity of biodegradable organic matter which, when released into the natural environment, will be biologically degraded, leading to the development of aerobic micro-organisms. This proliferation causes a drop in dissolved oxygen in the receiving environment, leading to asphyxiation of the species present. This analysis therefore enables us to assess the impact of the discharge on the receiving environment.

Biochemical oxygen demand (BOD) is the quantity of oxygen required to oxidize (biodegrade) organic matter by biological means (oxidation of biodegradable organic matter by bacteria).

It is used to assess the biodegradable fraction of the carbonaceous pollutant load in wastewater.

- PRINCIPLE :

BOD is measured after 5 days (=BOD₅), at 20°C (a temperature favorable to the activity of O₂-consuming micro-organisms) and in the dark (to avoid parasitic photosynthesis). Two samples are required: the first to measure the initial O₂ concentration, the second to measure the residual O₂ concentration after 5 days. BOD₅ is the difference between these 2 concentrations. Measurements are taken on the same volume, and the second sample is kept for 5 days in the dark at 20°C.

- PURPOSE :

- Determine the Biochemical Oxygen Demand in a water sample to be analyzed by 02 methods:

✓ Manometric method (respirometry) based on the principle of the WARBURG respirometer, in which a depression (decrease) in O₂ is directly recorded by a device (a volume of sample placed in ground-glass flasks).

✓ Dilution method.

MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:

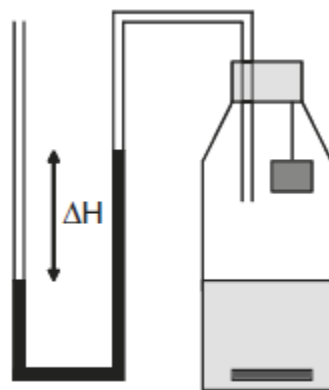
Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - Graduated pipette + pro-pipette - 100ml, 250ml volumetric flasks. - 500 ml beaker. - Stirrer + magnetic bar. - Thermometer or electro-metric probe. <u>Oxitop® BOD meter devices:</u> - 02 to 06 brown bottles. - Oxitop heads. - Rubber cups. - Gauged overflow flasks. - 20°C air-conditioned cabinet + agitator. 	<ul style="list-style-type: none"> - Sample water (industrial effluent) - Distilled water. - NaOH pellets, KOH or sodated lime. - N-allyl-thiourea (C₂H₈N₂S).

Diagram of a manometric measuring device :

There are 02 types of equipment on the market (see diagrams below).

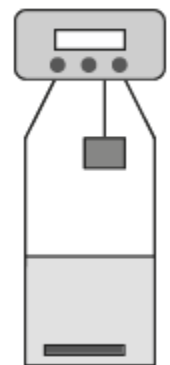
The oldest devices feature a manometric tube which is used to determine the vacuum corresponding to O₂ consumption. Newer devices use a cap fitted with a pressure sensor (OxiTop head) which automatically stores pressures at times 1, 2, 3, 4 and 5 days.

In all cases, the incubation flask is equipped with a shaking system and a pod containing KOH, which traps the carbon dioxide released during the biodegradation of oxidizable



1^{re} génération

(reducing) organic matter.



2^e génération

HANDLING (Operating mode) :

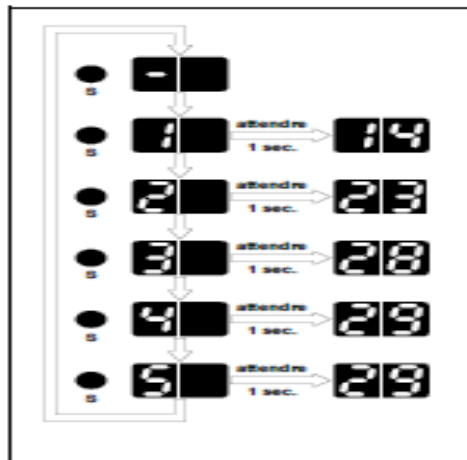
- 1- Rinse the brown bottle with the sample (domestic or industrial wastewater) to be measured. Drain well.
- 2- Homogenize the sample by shaking and aerating it to saturate it with dissolved air.
- 3- Start a measurement cycle by performing the following steps:

- a) Place in the bottles the volume of sample (effluent:domestic or industrialwastewater) determined on the basis of the scale to beused, measuredwith a graduatedcylinder.
- b) Place a magneticanchor (bar magnet) in eachbottle.
- c) Place sufficientabsorbers (causticpotash KOH in flakes or soda lime (CaO 65-80%+NaOH 5-20%+H₂O 6-18%(w/w)) in the alkali container or pod of eachbottle to fillitwithoutholesappearing on the sides.

NB : *If any of the absorber fallsinto the bottle, washitthoroughlybeforeinserting the sample to beexamined.*

- a) Place the bottles in their housings in the unit, screwing the caps on withoutclosingthemhermetically.
- b) Place the unit in the thermostaticcoolingchamber, set at the chosentemperature (20°C), to determine the D.B.O. Connect the magneticstirring system to the electrical power supply by pluggingitinto the socket (constant stirring). Activate the InnerSupply switch on the front panel of the thermostaticcooler.
- c) After approx. 30-40 minutes, the instrument and sampleshouldbe in thermal equilibrium at the selectedtemperature.
- d) Place and screw the D.B.O. Sensor onto the bottles. Reset eachmeasuring point (press and hold 02 buttons "M" and "S" simultaneously, to clearanyresidual memory), select the appropriatescale and restart the measuringcycle. La mesure va démarrer dès que la tête mesurera une température de 20 °C.
 - The oxitopwillautomatically record a value every 24 hours, for 5 days.
 - Duringthis time, to view the current value, press the "M" key (the key thatinformsyu of the measurementscale).

4- After the 05 days, readeach value by pressing the "S" key as follows :



5- Expression of results :

BOD₅ mgO₂/L = reading in the OxiTophead x conversion factor of BOD.

QUESTIONS :

- 1- Whatis the role of adding KOH or soda lime granules, if not NaOH?
- 2- In some cases of BOD measurement, a few pinches of allylthiourea (C₂H₈N₂S) are initiallyadded to the brownbottle. Why or whynot?
- 3- Fill in the following table with the results of yourmeasurements :

Type of water to be examined	Quantity of O ₂ (mg/L) measured daily by OXITOP at T=20°C					
	Au départ (0h)	1 st day (24h)	2 nd day (48h)	3 rd jour (72h)	4 th day (96h)	5 th day (120h)
Domestic wastewater (sewage)						
Industrial wastewater						
Water						

4-Draw the curve: Q_{O_2} (in mg/L)=f(time). (either with **Regressi®** software or on millimetric paper).
Comment.

5-Using the table in the APPENDIX, determine the BOD₅ value for each type of sample analyzed.

6-Calculate the **COD/BOD₅** factor for each type of sample analyzed. What does this ratio represent and what is its significance?

7- Apart from COD, what other parameters influence BOD₅?

8-Describe the dilution method (procedure) not used in this laboratory?

TP03 :
PHYSICO-CHEMICAL CHARACTERIZATION
OF WASTEWATER (TSS, Permanganate
Index)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 03:
PHYSICO-CHEMICAL CHARACTERIZATION OF
WASTEWATER (TSS, Permanganate Index)

- INTRODUCTION :

Organic matter, present in water and resulting from exchanges between the biosphere and the hydrosphere, can be a major source of pollution. While water is essential to life, it is also one of the main vectors of disease (gastro-enteritis, cholera, malaria...) and its decomposition can lead to the asphyxiation of aquatic fauna. Microbiological risk is an essential parameter to take into account. It is therefore necessary to assess this pollution and, above all, to reduce it, by analyzing water from domestic, agricultural or industrial discharges (waste) for the following physico-chemical and biological parameters:

- Particulate pollution :
 - Suspended solids (TSS)
- Pollution organic :
 - Chemical oxygen demand (COD)
 - Biochemical oxygen demand (BOD)
 - Permanganate index (PI)
- Pollution causing eutrophication :
 - Total nitrogen (NT)
 - Total phosphorus (TP)
- Pollution bacteriological :
 - Bacteria (total and fecal coliforms, Escherichia coli...etc)
 - viruses

- PURPOSE :

➤ Determination of the following parameters:

- Suspended solids (**part 1**)
- Permanganate index (**part 2**).

- MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:

Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - Graduated burettes 50ml or 25ml - Graduated pipette + pro-pipette - 1L, 100ml, 250ml volumetric flasks. 	<ul style="list-style-type: none"> - Sample water - Distilled water. - KMnO_4 ($2.0 \cdot 10^{-3}\text{M}$).

<ul style="list-style-type: none"> - Stirrer + magnetic bar. - Thermometer or electro-metric probe. - 1L graduated cylinder - 900ml, 250ml beakers + Large model funnel - Filterpaper (Wattman GFC-47mm glass microfibres) - Fiberglass funnel - Vacuum filtration equipment (vacuum flask + vacuum pump or water tube orifice + flexible hose) - <u>Reflux heating system</u> : - Flat-bottomed ground flask (150 or 250ml) + stopper. - Ball or serpentine refrigerant - Flexible hoses for water inlet and outlet - Balloon heater - Elevating support. - Stand for suspending flask and coolant 	<ul style="list-style-type: none"> - H₂SO₄ at (2M). - Sodium oxalate (Na₂C₂O₄ at 5.0.10⁻³M). - Pumice stones or boiling regulator beads. - Ice bath
---	---

- HANDLING (Operating mode) :

- Part 1 : TSS determination.

1- Introduce **300 ml** of sample water into a beaker (note the source or type of water sampled).

2- Carry out the following steps:

3- Remove coarse particles from the sample using a 5 mm square mesh sieve (AFNOR module no. 38) and, in the presence of fats and oils, homogenize the sieved water.

4- Introduce into a beaker: **V= 500 ml** of sample water (note source or type of water sampled).

5- Take a filterpaper (a GFC membrane) and mark it carefully so as not to damage it.

6- Weigh the filterpaper and note its mass **m₀** (in mg).

7- Place the filter (or membrane) on the filtration manifold (funnel).

8- Proceed with filtration, transferring the volume of water collected to the filterpaper.

9- Recover the filterpaper (membrane) after filtration, then place it in an oven at 105°C for **1h30 min** to remove excess water.

10- Weigh the membrane again, after drying, and record its mass **m₁** (in mg).

N.B : the volume filtered must not exceed 1L and filtration must not last more than half an hour

Expression of results:

$$MES(mg / L) = \frac{m_1 - m_0}{V(enL)}$$

Note: Retain water from filtration or centrifugation operations for determination of solids in solution.

➤ **Part 2 : permanganate index determination (IP).**

The permanganate index of water corresponds to the mass of oxygen "O₂" consumed by the oxidizable organic matter contained in 1.0 L of water. It is expressed in milligrams per liter.

- **Step 1:** A sample of water is oxidized in an acid medium, for 10 minutes at boiling point, by a solution of potassium permanganate in excess.

- Step2: Any remaining permanganate ions are reacted with an excess solution of ammonium oxalate.
- **Step3:** All remaining oxalate ions are reacted with the minimum volume of potassium permanganate solution.

- **HANDLING (Operating mode):**

Step1 :

- Introduce $V_{\text{éché}} = 25.0$ mL of the water studied, a bar magnet and 5.0 mL sulfuric acid (2 mol.L^{-1}) into a flask.
- Introduce a volume $V_1 = 20.0$ mL of a potassium permanganate solution S_1 ($\text{K}^+(\text{aq})$, $\text{MnO}_4^-(\text{aq})$) of concentration $C_1 = 2.0 \cdot 10^{-3} \text{ mol.L}^{-1}$ into the pouring funnel.
- Set up the water cooler vertically, with the pouring ampoule on its side. Start water circulation, agitation and heating (thermostat set to maximum). Pour in potassium permanganate solution when mixture begins to boil.
- Bring to a gentle boil (using pumice stones) for 10 minutes.

Step2 :

- Remove the ampoule and pipette in a volume $V_2 = 20.0$ mL of sodium oxalate solution S_2 ($2 \text{ Na}^+(\text{aq})$, $\text{C}_2\text{O}_4^{2-}(\text{aq})$), concentration $C_2 = 5.0 \cdot 10^{-3} \text{ mol.L}^{-1}$.

Step3 :

- When the solution is discolored, stop the water flow and pour the contents of the flask into an Erlenmeyer flask while the mixture (titrated solution) is still hot. Fill the graduated burette with solution S_1 .
- Place the Erlenmeyer on the magnetic stirrer and start titrating your mixture while slowly pouring in solution S_1 . Stop adding solution when the pink tint persists for more than 30 seconds.
- Then record the volume V_{E1} of solution S_1 poured in as the equivalent volume (volume for which permanganate and oxalate ions are completely consumed).

➔ **NB : blank test (in parallel)**

- Follow the same procedure as in the previous three steps, but use 25ml of distilled water instead of the water sample (effluent).

- **QUESTIONS :**

➤ **Part (1) : determination of physicochemical parameters in wastewater.**

1- Indicate the importance of determining the following physicochemical parameters (indicate the information provided by each parameter analyzed):

TSS, COD, BOD₅, NT or NTK, PT.

3- Fill in the following table -1- with the results obtained during the measurements carried out :

Type of water to	TSS	COD (TP01)	BOD ₅ (TP02)
------------------	-----	------------	-------------------------

beexamined	(mg/L)	(mgO ₂ /L)	(mgO ₂ /L)
Wastewater 1			
Wastewater2			
River water			
Water			

3- from the analyses obtained, calculate the following ratios and indicate their significance in the following table:

Type of water to beexamined→	Wastwater 1	Wastwater 2	Water	Importance or information provided by this report
COD/BOD(biodegradability index)				

➤ **Partie 2 :determination of permanganate index (IP)**

1- Write down the redox half-equations for MnO₄⁻(aq)/Mn²⁺(aq) and CO₂(aq)/C₂O₄²⁻(aq). Deduce the equation for the reaction between permanganate and oxalate ions in an acid medium.

2-

2.a. Draw up progress tables for the reactions in steps 2 and 3, noting :

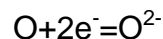
- n₁ the quantity of permanganate ions introduced into the Erlenmeyer flask;
- n₀ the quantity of permanganate ions reacted with the organic matter;
- n₂ the quantity of oxalate ions introduced into the Erlenmeyer flask
- n_{rest} the quantity of oxalate ions remaining at the start of step 3
- n_E the quantity of permanganate ions added for V = V_E (step 3).

2.b. Show that :
$$n_0 = n_1 - \frac{2}{5} \cdot n_2 + n_E$$

2.c. Deduce that n₀ = n_E then calculate n₀.

3.a. Deduce the quantity n_e of electrons used to oxidize organic matter.

3.b. Calculate the quantity and then the mass of oxygen "O" that would react with these electrons according to the half-equation:



3.c. Deduce the permanganate index of the sample.

NB :To determine the value of volume V_2 , the concentration (or titre) of potassium permanganate used as the titrating solution must be verified

TP04 :
COAGULATION-FLOCCULATION TEST
(Jar-test)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 04 :
COAGULATION-FLOCCULATION TEST
(Jar-test)

- INTRODUCTION :

The coagulation-flocculation process facilitates the removal of suspended solids and colloidal particles

The coagulation-flocculation process facilitates the removal of suspended solids and colloidal particles (sizes below $1\mu\text{m}$), which is why coagulation-flocculation can be used in the water treatment process to reduce turbidity. To treat water for potabilization, the coagulation-flocculation process requires rigorous elimination of flocs, and must be coupled with decantation. Reagents must be precisely dosed to avoid residual matter in the produced water.

Coagulation (the destabilization of colloidal particles by the addition of a chemical reagent known as a coagulant) eliminates repulsions linked to the electronegativity of colloids. This is achieved by adding electropositive metal salts, which bind to the colloids and neutralize them, thus canceling the Zeta potential (Characteristic of the repulsive forces between particles. Determined by measuring the displacement velocity of a particle subjected to an electric field) of these colloids.

Secondly, flocculation causes colloidal particles to agglomerate. Because of their low weight, individual particles are unable to settle, and by creating agglomerates (known as flocs), we can significantly increase the weight of the particles, making them large enough to settle.

Factors that can improve coagulation-flocculation are :

- time and velocity gradient are important for increasing the probability of particle clashes.
- and pH is a very important factor for colloid removal.

- PURPOSE :

- Determine the optimum dose of coagulant and optimize the pH value to ensure that the coagulation-flocculation process is effective in treating polluted water (effluent).

- MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:

Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - Graduated pipette + pro-pipette - 100ml, 250ml and 1L volumetric flasks. - 06 beakers (900 ml). - Thermometer or electro-metric probe. 	<ul style="list-style-type: none"> - Sample water (polluted) - Distilled water + bentonite - $\text{Al}_2(\text{SO}_4)_3 \cdot 18\text{H}_2\text{O}$ at 10g/L - FeCl_3 at 10g/L

- pHmeter. - Turbidimeter.	- Polyelectrolyte at 1g/L - HCl 1M - 1M NaOH
-------------------------------	--

- HANDLING (Operating mode) :

✓ **Part1 :Finding the optimal coagulant dose**

6- Prepare 3L of a clay suspension (bentonite) at 200 mg/L or take 3L of polluted water for treatment.

7- Prepare 100ml of a solution of $Al_2(SO_4)_3 \cdot 18H_2O$ at 10g/L (coagulant-1) or $FeCl_3$ at 10g/L (coagulant-2), $FeSO_4$ at 10g/L (coagulant-3), $CuSO_4$ at 10g/L (coagulant-4). Introduire dans chaque bécher de 900ml :

Sample (Beaker no.)	1 (witness)	2	3	4	5	6	7
Volume of polluted water (ml)	500	500	500	500	500	500	500
Coagulant volume-1 or 2, 3 or 4 « V_p » à 10g/L	0ml	2,5ml	5ml	7,5ml	10ml	15ml	20ml

3-Measure pH and turbidity (T_0) of sample 1 (control).

4- Place the 06 beakers under rapid agitation (150 rpm) for 3 min.

5-Reduce agitation to 40 rpm for 15 min (or 30 rpm for 20 min) and observe, from time to time, for floc formation and quality.

6- Stop stirring and leave the mixture to stand for 30 min.

7- Pipette approximately 50 ml of supernatant to measure turbidity (T_i) and final pH.

8-Filter on pre-weighed filter paper (m_0), dry at 110°C and weigh the quantity of sludge obtained ($m_1 - m_0$).

✓ **Part 2 :Finding the right pH for coagulation-flocculation operation**

1- Prepare 3L of a clay suspension (bentonite) at 200 mg/L or take 3L of polluted water for treatment.

2- Prepare 100ml of a solution of $Al_2(SO_4)_3 \cdot 18H_2O$ at 10g/L (coagulant-1) or $FeCl_3$ at 10g/L (coagulant-2), $FeSO_4$ at 10g/L (coagulant-3), $CuSO_4$ at 10g/L (coagulant-4).

3- Introduce into each 900ml beaker, adjusting pH with HCl acid solution (1M) and NaOH base solution (1M):

Sample (Beaker no.)	1	2	3	4	5	6	7
Volume of polluted water	500	500	500	500	500	500	500

(ml)							
Coagulant volume-1 or 2, 3 or 4 « V_p » à 10g/L (optimum dose)	2.5ml	2,5ml	2.5ml	2.5ml	2.5ml	2.5ml	2.5ml
pH _{initiale}	6	7	8	9	10	11	12

Place the 06 beakers under rapid agitation (**150 rpm**) for **3 min**.

5- Reduce agitation to **40 rpm** for **15 min** (or 30 rpm for 20 min) and observe, from time to time, for floc formation and quality.

6- Stop stirring and leave the mixture to stand for **30 min**.

7- Pipette approximately 50 ml of supernatant to measure turbidity (**Ti**) and **final pH**.

- **QUESTIONS :**

1- Fill in the following table: **(partie-1)**

Sample (Beaker no.)	1 (témoin)	2	3	4	5	6
Coagulant volume-1 or 2, 3 or 4 « V_p » à 10g/L	0ml	2,5ml	5ml	7,5ml	10ml	15ml
Coagulant dose -1 or 2, 3 or 4 " C_f " (mg/L)
pH _{finale}
Turbidity « T_i » (NTU)
$(T_0 - T_i) \times 100 / T_0$ (efficiency)
TSS (mg/L)

2- Plot in the same graph: (either with **Regressi®** software or on millimetric paper)

- **pH_{finale} = f(C_f)**

- **T_i = f(C_f)**.

3- Deduce the value of the optimum dose (C_{optim} in mg/L) of the coagulant used to treat the polluted water.

4- Plot in the same graph: (either with **Regressi®** software or on millimetric paper)

Max Efficiency = f(C_f of each coagulant) or **Max Efficiency = f(coagulant type)**.

5- Provided you've carried out the experiment with all 04 coagulants. Which of these 04 is the most effective for this type of water treated by the coagulation-flocculation test?

6- Fill in the following table with the results obtained during the measurements carried out: **(part-2)**

Sample (Beaker no.)	1	2	3	4	5	6
Coagulant volume-1 or 2, 3 or 4 « V_p » à 10g/L (optimum dose)	2.5ml	2,5ml	2.5ml	2.5ml	2.5ml	2.5ml
pH _{finale}
Turbidity « T_i » (NTU)

$(T_0 - T_i) \times 100 / T_0$ (efficiency)
---	-------	-------	-------	-------	-------	-------

7- Plot in the same graph: (either with **Regressi®** software or on millimetric paper)

$T_i = f(\text{pH}_{\text{final}})$

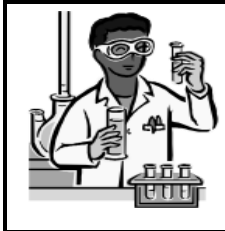
8- Deduce the optimum pH value?

9- Conclude.

TP05 :
DECANTATION TEST-Part 1
(KYNCH's Law)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 05 :
DECANTATION TEST-Part 1
(KYNCH's Law)

- INTRODUCTION :

There are two types of settling:

- **Settling of discrete particles (grit):** of the same size and origin.
- **Decantation of flocculent particles:** the falling speed of flocculent particles increases as particle agglomeration increases.

✓ *Settling of discrete particles:*

Discrete particle settling consists in eliminating particles of the same size and origin.

As the particle falls, it is subjected to three forces

- The force of gravity.
- Archimede thrust.
- Frictional forces.

There are various formulas for calculating the falling speed of a particle, depending on the flow regime (Reynolds number) in the settling tank. Different formulas for calculating fall velocity as a function of Reynolds number Re :

- For $10^{-4} < Re < 1$ (laminar regime for free-surface flows), the falling velocity is given by Stokes' formula:

$$V_p = \frac{d^2 \cdot (\rho_p - \rho_l) \cdot g}{18 \cdot \mu}$$

where: d : particle diameter, μ : dynamic viscosity of liquid, ρ_p : particle density and ρ_l : liquid density.

- For $1 < Re < 500$, intermediate case equation:

$$V_p = \frac{0,153 \cdot g^{0,71} \cdot d^{1,14} \cdot (\rho_p - \rho_l)^{0,71}}{\rho_l^{0,29} \cdot \mu^{0,43}}$$

- For $500 < Re < 10000$; **Newton's** equation (for turbulent flow):

$$V_p = 1,74 \cdot \sqrt{\frac{g \cdot d \cdot (\rho_p - \rho_l)}{\rho_l}}$$

✓ **Decantation of flocculent particles:**

The sedimentation rate of particles increases during settling, due to particle agglomeration. Different mathematical models describe this type of settling.

There are 02 types of flocculated particles settling:

- ⇒ Diffuse settling (during settling, flocculation continues and V_p velocity increases when the concentration of flocculated matter is between 50-500 mg/L).
- ⇒ Piston settling (when the concentration of flocculated particles > 500mg/L, interactions between the particles are not negligible, so they settle at piston → flocculation and settling can be improved first, then slowed down beyond a certain critical concentration, referred to as "slowed settling").

- **PURPOSE :**

Study vertical-flow piston settling of flocculated particles and plot the "kynch" curve.

- **MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:**

Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - 02 Glass measuring cylinders 1L or 2 L - Graduated pipette + pro-pipette - 100ml, 250ml and 1L volumetric flasks. - 04 900 ml beakers. - 03 Jar-test flocculators - Stopwatch 	<ul style="list-style-type: none"> - Distilled water. - Bentonite 5g/L and 10g/L or other clay. - $Al_2(SO_4)_3 \cdot 18H_2O$ at 10g/L (coagulant 1) - $FeCl_3$ at 10g/L (coagulant 2)

- **HANDLING (Operating mode) :**

1- Prepare 1L of a clay suspension (bentonite) at 5g/L and 10 g/L each, or take 1L of sludge-laden polluted water for treatment.

2- Prepare 100ml of 10g/L $Al_2(SO_4)_3 \cdot 18H_2O$ (coagulant-1) or 10g/L $FeCl_3$ (coagulant-2) solution.

3- Introduce into each 900ml beaker :

Sample (Beaker no.)	Bentonite (5g/L)		Bentonite (10g/L)	
	1	2	3	4
Volume of polluted water (ml)	500	500	500	500
Coagulant volume-1 or 2, « V_p » à 10g/L (optimum dose)	2.5ml	2,5ml	2.5ml	2.5ml

1- Place the 04 beakers under rapid agitation (**150 rpm**) for **3 min**.

2- Reduce agitation to **50 rpm** for **15 min** (or 30 rpm for 20 min) and observe from time to time to detect floc formation and quality.

3- Stop stirring and transfer each 02 beakers (2x 500ml suspension) directly into a 1L glass measuring cylinder.

4- Start the stopwatch when the last drop of suspension is poured in.

5- During the decanting operation, record the time "**t**" continuously in each test tube and read the volume (or height "**H**") at the moment of appearance of each interface formed between the particles and the clear liquid (water).

NB :don'tforget to take the dimensions (height "H" of the 1L test tubes and their diameters "d") whichwillbeuseful for the vertical flow decantationoperation.

- **QUESTIONS :**

1- Fill in the table with the resultsobtainedduring the measurements:

Test tube N° ① : →	Bentonite (5g/L) + 2.5ml de coagulant 1 ou 2		Test tube N° ② : →	Bentonite (5g/L) + 2.5ml de coagulant 1 ou 2	
Time(sec)	Volume read(ml)	Height « H » (m)	Time (sec)	Volume read(ml)	Height « H » (m)
t ₀ =0.00	1000	H ₀ =	t ₀ =0.00	1000	H ₀ =
t ₁ =.....			t ₁ =.....		
t ₂ =.....			t ₂ =.....		
t ₃ =.....			t ₃ =.....		
t ₄ , t ₅ , t ₆			t ₄ , t ₅ , t ₆		

NB :itispreferable to use the **Regavi**® software afterfilming all the settlingoperationscarried out in the Laboratory (to ensureproper monitoring of the settlingoperation and, above all, good observation of the fall of particles, as well as accuratereading of volume and height).

2- Draw the 02 graphs: (eitherwith**Regressi**® software or on millimetricpaper)

- **H= f(t) (kynchcurve)** and **V=(t)**. forspecimens ① and ②.

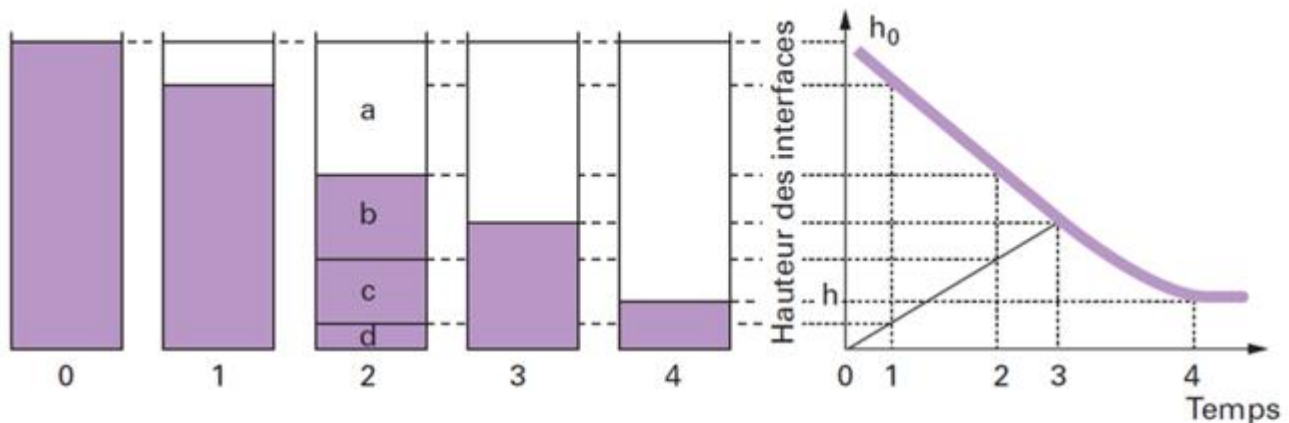
3- Interpret the 02 graphs (indicatewhetherthereis a flake coalescence phase) see APPENDIX .

4- Graphicallydeduce the velocity "V" at which the particlesfallinto the 02 test tubes (seeAPPENDIX).

5- Are thereothermethods of studying the settling of flocculatedparticles? If so, please list them.

APPENDIX

When piston decantation is performed in a tube of sufficient height and diameter (at least a one-liter test tube), four zones are generally observed (Figure 1).



a : Zone de clarification où le liquide est clair.

b : Zone de suspension homogène de même aspect que la solution de départ avec une interface a-b nette.

c : Zone de transition (pas toujours observable).

d : Zone d'épaississement des boues dont le niveau augmente rapidement avant de diminuer lentement.

Figure 1: Piston decantation: Kynch curve

At a certain point, zones b and c disappear - this is the critical point. The evolution of the height of the a-b interface as a function of time forms the Kynch curve.

⇒ ***Kynch curve***: (figure 2)

Kynch's fundamental hypothesis is that the speed at which a particle falls depends only on the local concentration C of particles.

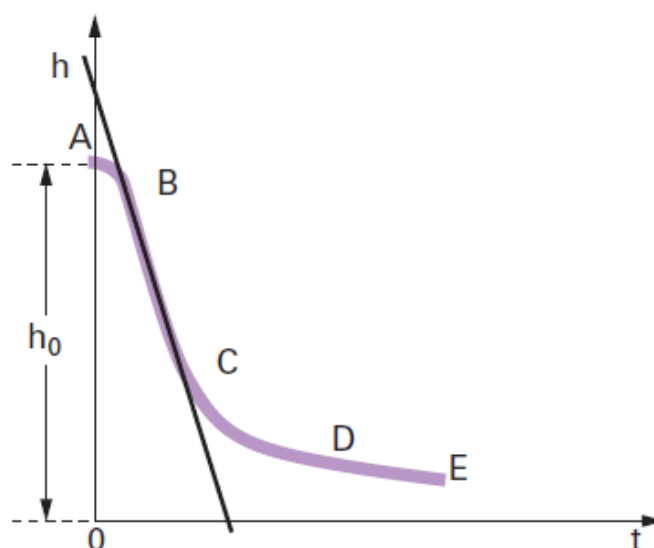


Figure 2. Kynchcurve

From A to B, the separation surface is more or less clear: this is the flake coalescence phase. This phase is sometimes non-existent.

From B to C, a rectilinear section translates into a constant falling speed V (slope of the straight line). For a tube of given dimensions, V is a function of the initial TSS concentration and the flocculation characteristics of the suspension. As the initial concentration C increases, the settling velocity V of the mass decreases: for example, for an urban activated sludge whose TSS concentration increases from 1 to 4 g - L⁻¹, V decreases from 6 to 1.8 m - h⁻¹.

The upwardly concave CD section corresponds to a gradual slowdown in the rate of fall of the top layer of the deposit.

From D onwards, the flakes touch each other, exerting compression on the lower layers.

Kynch's theory applies to the BC and CD sections, which cover the essential area of flocculated sludge settling.

⇒ **Interpretation:**

If we consider a suspension whose settling does not include a coalescence phase (Figure 3), the calculation shows that :

- in the BOC triangle, concentration and fall velocity are constant and equal to the initial values prevailing in B ;
- in the COD triangle, the equi-concentration curves are straight lines passing through the origin, which means that from the very first moments of settling, the layers closest to the bottom pass through all the concentrations between the initial concentration and that corresponding to point D, the start of compression.

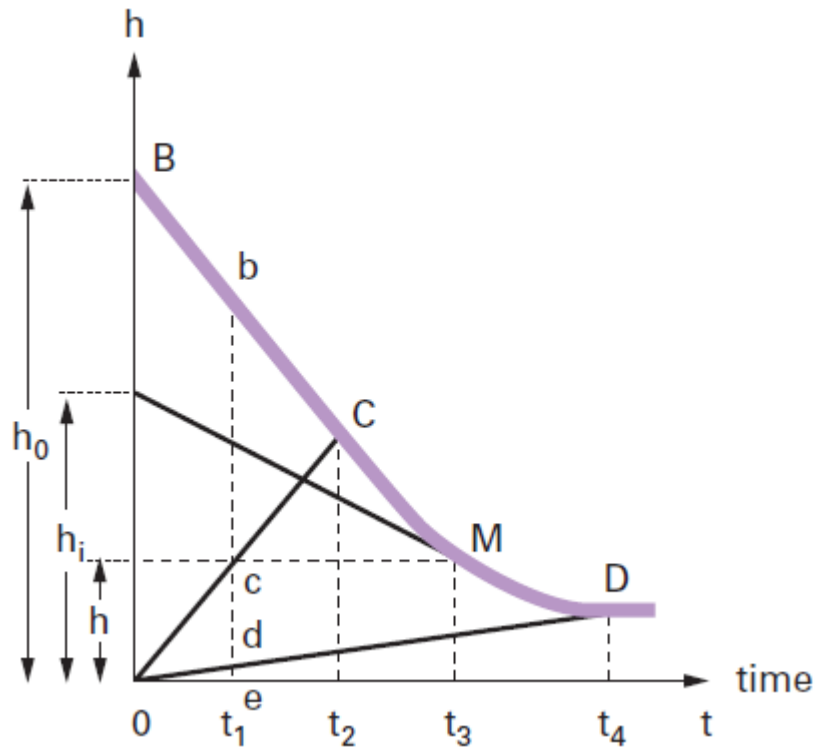


Figure 3. **Interpretation**

The muddy medium of height h at time t_1 therefore has three distinct zones:

- an upper zone bc where concentration and fall velocity are uniform and have retained their initial values C and V_0 ;
- an intermediate zone cd in which concentration increases progressively from c to d , and fall velocity decreases accordingly;
- a lower zone de where the sludge flakes are subjected to compression.

In the medium considered, the upper zone disappears at time t_2 , and only the lower zone remains at time t_4 .

For point M in part CD , two concentrations can be defined:

- C_M^i interface concentration,
- C_M average concentration.

According to Kynch's hypothesis :

$$C_M^i = C_0 \cdot \frac{h_0}{h_i}$$

In addition :

$$C_M = C_0 \cdot \frac{h_0}{h}$$

The three parts BC , CD and DE of the Kynch curve (Fig. 2) are applied to the calculation of slow sedimentation structures. Phase BC corresponds to sludge-contact decanters.

The CD phase relates to structures where sludge concentration is required (thickened sludge recirculation devices). The DE phase is used for sludge thickening.

TP06 :
DECANTATION TEST-Part 2
(MOHLMAN Index and DSVI)



MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 06 :
DECANTATION TEST-Part 2
(MOHLMAN Index and DSVI)

- INTRODUCTION :

The treatment sludge formed is obtained after the coagulation-flocculation reaction or biological treatment with activated sludge. Its quantity and settleability (solid-liquid separation) can be estimated using the Mohlman index. In general, an easily settleable sludge has a Mohlman Index (MI) of between 50 and 150 mL/g, with a TSS concentration in the sludge of between 1,500 and 2,500 mg/L.

The MOHLMAN "I_M" (Sludge Volume Index) is defined as the volume occupied after 30 minutes settling of a sludge sample corresponding to 1 gram of dry matter.

This index is represented by the ratio: volume of sludge settled in 30 minutes (mL/L) / mass of dry matter (g/L).

- The MOHLMAN index is used to characterize sludge dilatability,

*A normal sludge has an index of 100. In the presence of bulking, the index increases, reaching a value of 500.

- If there are problems with clarifier settling, the sludge should be examined microscopically. is defined as the volume occupied after 30 minutes settling of a sludge sample corresponding to 1 gram of dry matter.

This index is represented by the ratio: volume of sludge settled in 30 minutes (mL/L) / mass of dry matter (g/L).

- The MOHLMAN index is used to characterize sludge dilatability,

*A normal sludge has an index of 100. In the presence of bulking, the index increases, reaching a value of 500.

- If there are problems with clarifier settling, the sludge should be examined microscopically.

- The MOHLMAN index is only truly representative of a sludge's dilatability if :

*the final volume obtained, from an initial volume of 1L, is between 100-250mL. In this range, the index is proportional to the sludge concentration.

L'indice de boues « I_B » (ou Diluted Sludge Volume Index) est défini à partir de tests de décantation permettant d'obtenir des volumes de boues compris entre 100-250mL

- PURPOSE :

- Determine the **MOHLMAN index (I_M or SVI)** of water from the aeration tank.

- Determine the **Sludge Index (I_B or DSVI)** of water from the aeration tank.

- MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:

Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - 04 IMHOFF cone or 04 1L glass measuring cylinders - Graduated pipette + pro-pipette - 100ml, 250ml and 1L volumetric flasks. - 04 900ml beakers. - Filter paper - Funnels (GM) - Stopwatch. - Data processing software (Regavi®, Avimeca®.....etc) 	<ul style="list-style-type: none"> - Distilled water. - Muddy water (sludge) from aeration tank after 15 or 20 min of operation. - Bentonite 5g/L and 10g/L or other clay.

- HANDLING (Operating mode) :

Important note:

Beforehand, measure the "TSS" of the muddy water (sludge) coming from the aerator (take an aliquot) see TP01 on physicochemical and biological treatment of wastewater.

8- Perform the following operations:

➤ **Part A :determination of the MOHLMAN index (I_M or SVI).**

- a- a- Transfer the slurry to a 1000 mL test tube or IMHOFF cone.
- b- b- Allow to settle and monitor sludge height every 5 minutes.
- c- c- Determine the volume of sludge at **t = 30 minutes.**



Figure 1: IMHOFF cone

Expression of results:

$$I_M = \frac{V_{30}}{MES}$$

V_{30} ou V :volume of sludge after 30 min settling (cm^3 or ml),

MES or (TSS) : present in this volume (g).

➤ **Part B :determination of the sludge index (IB or DSVI).**

a- Introduce into each 1000ml test tube:

Sample (Test piece no.)	①	②	③	
STEP-Sidi Bel Abbas	Volume of muddy water (ml) in aeration tank	500	250	125

- b- Fill test tubes to 1 L with water taken from the clarifier outlet (secondary clarifier).
- c- Homogenize the contents of the test tubes by inverting them several times after sealing.
- d- Let settle after 30 min.
- e- Start the stopwatch when the last drop of suspension is poured.
- f- During the decanting operation, record the time "t" continuously in each test tube and read the volume (or height "H") at the moment of appearance of each interface formed between the particles and the clear liquid (water).

NB : don't forget to take the dimensions (height "H" of the 1L test tubes and their diameters "d") which will be useful for the vertical flow decantation operation.

Expression of results:

$$I_B = \frac{V_{30}}{(MES)_a \cdot f}$$

V_{30} ou V : sludge volume after 30 min settling (cm^3/L or ml/L),

$(MES)_a$ or (TSS) : present in this volume (g/L dry matter).

f : dilution factor (**volume of sludge initially introduced into the test tube in $ml/1000$**)

QUESTIONS :

1- Fill in the following table with the results obtained during the measurements carried out:

Nature of wastewater to be examined	m_0 (in mg)	m_1 (in mg)	TSS (mg/L)
Aeration tank water			
..... etc			

2- Calculate the MOHLMAN index " I_M " (ml/g).

3- Based on the "IM" value obtained, is it necessary to move on to measuring "IB"?

4- Define the **bulking** problem.

5- This parameter is used to size one of the wastewater treatment stages. Which one?

6- This index is useful for determining another parameter characterizing the sludge. Which is it?

7- Fill in the table with the results obtained during the "IB" measurements:

Test tube N° ① : →	500ml muddy water + q.s.p 1L water.		Test tube N° ② : →	250ml muddy water + q.s.p 1L water.		Test tube N° ③ : →	125ml muddy water + q.s.p 1L water.	
Time (sec)	Volume read(ml)	Height « H » (m)	Time (sec)	Volume read(ml)	Height « H » (m)	Time (sec)	Volume read(ml)	Height « H » (m)
$t_0=0.00$	1000	$H_0=....$	$t_0=0.00$	1000	$H_0=....$	$t_0=0.00$	1000	$H_0=....$
$t_1=.....$			$t_1=.....$			$t_1=.....$		
$t_2=.....$			$t_2=.....$			$t_2=.....$		
$t_3=.....$			$t_3=.....$			$t_3=.....$		
$t_4, t_5, t_6.....$			$t_4, t_5, t_6.....$			$t_4, t_5, t_6.....$		

NB : it is preferable to use the **Regavi®** software after filming all the settling operations carried out in the Laboratory (to ensure proper monitoring of the settling operation and, above all, good observation of the fall of particles, as well as accurate reading of volume and height).

2- Plot the graph: (either with Regressi® software or on millimetric paper)
 $H = f(t)$ (kinch curve) or $V = f(t)$. for test specimens ① and ② and ③.

3- Determine the "IB" (DSVI) of each test piece by filling in the following result table:

	Sample (Test piece no.)	①	②	③
Aeration tank water	f (dilution factor)			
	V30			
	(TSS) _{B.aeration}			
	I _B (DSVI) in ml/g			

4- Conclude (what is the settling quality of this muddy water? good, average, poor) - see APPENDIX.

APPENDIX

Mohlman Index (sludge volume index : SVI)

A particular point is considered on the Kynch curve, that of the 30-minute abscissa: the **Mohlman index** " I_M " is widely used to characterize the settleability of biological sludge and therefore for clarifier sizing, or even the triggering of corrective methods if overflow develops.

$$I_M = \frac{V_{30}}{MES}$$

V_{30} or V : volume of sludge after 30 min settling (cm^3 or ml),
MES or (TSS) : present in this volume (g).

The disadvantage of Mohlman's index is that it is highly dependent on the initial sludge concentration. Methods have therefore been proposed to define an index that is independent of this concentration, and therefore characteristic only of the state of the sludge in the plant.

These are :

(IB) or diluted Mohlman index (DSVI).

The Kynch curve is determined after dilutions to recover a sludge volume, after 30 min settling, in the vicinity of 200-250 mL per L.

The "DSVI" sludge index used in France is valid if this volume is between 100 and 300 mL, the DSVI used by the Anglo-Saxons if it is between 150 and 250 mL. In both cases, activated sludge can be said to have **very good settleability** when its sludge index or DSVI is between 50 and 100 cm^3g^{-1} , **normal settleability** between 100 and 200, and **poor settleability** above 250.

TP07 :
DISINFECTION TEST
(chlorinedemand - "break point" method)

MASTER 2: ENVIRONMENTAL PROCESS ENGINEERING
TP: PHYSICO-CHEMICAL AND BIOLOGICAL TREATMENT OF WASTEWATER



TP N 07 :
DISINFECTION TEST
(chlorinedemand - "break point" method)

- INTRODUCTION :

This is the final stage in the treatment chain, eliminating all pathogenic micro-organisms from the water, as well as some organic and mineral pollution. A few common germs may remain in the water, as disinfection is not sterilization.

Chlorine is used for disinfection, so a certain level of residual chlorine must be injected to kill any germ that can be revived.

It is generally accepted that disinfection is the final stage in a treatment chain, where chlorine penetrates micro-organisms such as bacteria or viruses and destroys them by inhibiting certain vital synthesis reactions. Many environmental factors influence the effectiveness with which chlorine disinfects water, including water temperature, pH, contact time, degree of mixing, turbidity, undesirable substances and available chlorine concentration.

The contact time or action time of sodium hypochlorite is at least half an hour, but if the temperature is only between 10 and 18°C, the contact time must be at least one hour, and longer if the temperature is below 10°C.

Below is the curve representing the "breakpoint" test to determine the optimum chlorine dose needed to eliminate all the nitrogenous matter (organic and mineral) that gives our treated water an unpleasant taste.

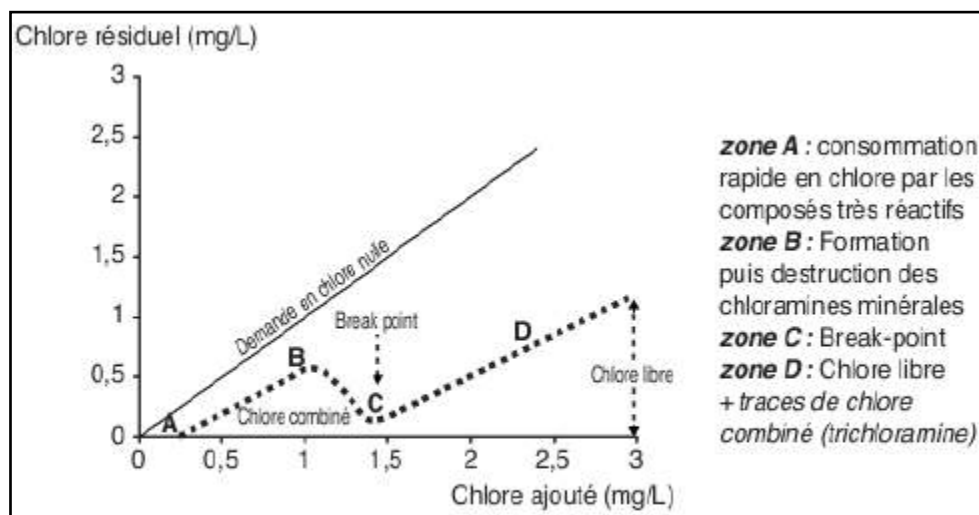


Figure 2 : curve representing the break point of disinfected natural water.

This curve (Figure 1) is subdivided into 03 zones:

1st zone: represents the increase in residual chlorine due to the formation of chloramines and organochlorines.

2nd zone: shows the decrease in residual chlorine due to the destruction of chloramines.

3rd zone: reveals the quasi-linear growth of residual chlorine due to the formation of free chlorine effective for disinfection.

- PRINCIPLE :

Residual chlorine in water is often analyzed by the volumetric or iodometric method, the latter involving a highly acidic medium ($3 < \text{pH} < 4$) by introducing iodide ions (I^- , transparent color), then dosing the iodine (I_2 , yellow color) released by sodium thiosulfate ($\text{Na}_2\text{S}_2\text{O}_3$). This enables chlorine in Cl_2 form to be determined. The results correspond to oxidizing equivalents (HClO , ClO^-) expressed in mgCl_2/L .

- PURPOSE :

Determine the precise dose of chlorine required for a volume V of water using the **break-point method** (total degradation of ammoniacal nitrogen - lowest residual chlorine value).

- MATERIALS, MEASURING EQUIPMENT AND PRODUCTS:

Materials, Measuring equipment	Products
<ul style="list-style-type: none"> - 02 Graduated burettes - 02 Graduated micro-burettes - Graduated pipettes + pro-pipette - 100ml, 250ml and 1L volumetric flasks. - 20 Erlenmeyer flasks or 150ml flasks. - Magnetic stirrers - Magnetic stirrers 	<ul style="list-style-type: none"> - Distilled water. - Surface or dam water or treated water. - Sodium thiosulfate (0.01M). - Sodium thiosulfate (0.1M). - Potassium iodide 0.1M (KI). - Starch starch (10g/L). - Glacial CH_3COOH (5M). - H_2SO_4 (1M) - Bleach ($\text{Ch}^\circ 12$)

- HANDLING (Operating mode):

- Important note:

Carry out a chlorometric control (Chl°) of the bleach you are going to use to determine the breakpoint.

Perform the following operations :

➤ **Part A : control of chlorometric degree (Chl°) of bleach**

1- From the commercial bleach solution (S_0) of concentration C_0 , prepare 100ml of a solution (S) of concentration $C = C_0/10$. (10 times diluted).

2- Into an Erlenmeyer flask, introduce :

- 10ml solution (S).
- 10 ml glacial acetic acid (5M) or sulfuric acid (H_2SO_4), concentration 1M.
- 20 ml potassium iodide solution (KI), concentration $C_1 = 0.1\text{M}$.

3- Introduce a bar magnet and a few drops of starch paste. Homogenize the mixture using a magnetic stirrer.

4- Fill burette with sodium thiosulfate solution ($\text{Na}_2\text{S}_2\text{O}_3$) with $C_2 = C_{\text{S}_2\text{O}_3} = 0.1\text{M} = 0.1\text{N}$.

5- Gradually add sodium thiosulfate until the mixture is discolored to the drop. Note the volume poured $V_e(\text{A})$ or $V_e(\text{S}_2\text{O}_3-2)$.

Expression of results:

$$[Cl_2]_{Actif} (g / L) = \frac{C_{S_2O_3^{-2}} V_{e(S_2O_3^{-2})}}{V_{\text{echantillon-eau-javel-dilué}}} (M_{Cl_2} / 2)$$

Or

$$[Cl_2]_{Actif} (mg / L) = 35,5 * 10^3 \frac{C_{S_2O_3^{-2}} V_{e(S_2O_3^{-2})}}{V_{\text{echantillon-eau-javel-dilué}}}$$

$V_{e(A)}$ or $V_{e(S_2O_3^{-2})}$: volume of sodium thiosulfate ($Na_2S_2O_3$) added at equivalence point (ml),

V_{sample} : volume of diluted bleach test sample (ml)

$M(Cl_2) = (35.5 * 2) = 71 \text{ g.mol}^{-1}$

Thus: (with bleach dilution factor = 10 times)

$$C_0 (mg / L) = 10. \left[35,5 * 10^3 \frac{C_{S_2O_3^{-2}} V_{e(S_2O_3^{-2})}}{V_{\text{echantillon-eau-javel-dilué}}} \right]$$

Hence :

$$Chl^{\circ} = \frac{C_0 (mg / L_{\text{eau-javel}})}{3,17.10^3 (mg / L_{\text{eau-javel}})}$$

➤ **Part B :chlorine residual measurement (break-point test)**

a- This time, fill the burette with sodium thiosulfate solution ($Na_2S_2O_3^{-}$ 0.01N).

b- According to the following table, introduce into each beaker or Erlenmeyer flask (150ml): (the 15chl° bleach used is 100 times diluted (solution "S" i.e. 0.48 g/L).

NB : for bleach with chlorometric degrees other than 15 chl°, the volumes to be withdrawn are listed in APPENDIX.

Samples → (bekers N°)	①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
Volume (V'p) of Cl ₂ added at 100 ml treated water	0.105	0.157	0.210	0.315	0.368	0.420	0.630	0.841	1.051	1.261
Samples → (bekers N°)	⑪	⑫	⑬	⑭	⑮	⑯	⑰	⑱	⑲	⑳
Volume (V'p) of Cl ₂ added at 100 ml treated water	1.472	1.682	1.892	2.103	2.313	2.523	2.734	2.944	3.154	4.206

a- Shake and cap Erlenmeyer flasks or beakers.

b- Place the Erlenmeyer flasks or beakers in a dark place.

c- Leave these flasks (Erlenmeyer flasks or beakers) for a defined contact time (here 30 min or 1h).

d- Take from each beaker or Erlenmeyer :

- 10 ml chlorine-treated water sample

- 20 ml sulfuric acid (H_2SO_4 , 1M) or 20 ml glacial acetic acid (CH_3COOH , 5M).
- 20 ml potassium iodide solution (KI), concentration $C_1 = 0.1M$.

e- Perform volumetric titration of all prepared solutions with sodium thiosulfate titrant solution ($Na_2S_2O_3$, 0.01M) until the yellow color disappears (or the blue color disappears if you used 10g/L starch).

f- Note the volume poured at equivalence $V_{e(B)}$

NB : To find out how much bleach to add to achieve the desired concentration, you need to know the chlorometric value, which should be indicated on the bottle (although beware of the reliability of this information and of counterfeiting in some countries).

One chlorometric degree corresponds to \rightarrow 3.17 grams of active chlorine per liter of bleach under C.N.T.P. conditions (1atm and 273°K).

Therefore, if the bleach available is at Chl° , and if you wish to obtain a concentration "C" or $[Cl]_{Active}$ or Added in mg/L of active chlorine in the water to be treated (between 5 and 20mg/L, depending on the case), the volume of bleach to be added can be easily calculated using the following formula:

$$V_{bleach} \text{ (ou } V_p) = C * V_{water\ treated} / (3,17 * 10^3 * chl^\circ)$$

The result obtained is in ml if the concentration was expressed in mg/L.

- ✓ If the bleach is diluted "n times", the new volume to be added is calculated using the following formula:

$$V'_{eau\ de\ javel} \text{ (ou } V'_p) = n * V_{eau\ de\ javel}$$

- QUESTIONS :

➤ Part A : control of chlorometric degree (Chl°) of bleach

- Fill in the following table of results: (the 15 chl° bleach used is 10 times diluted ("S" solution, i.e. 4.8 g/L).

$V_{e(A)}$ in ml	$[Cl_2]_{actif}$ diluted in mg/L	C_0 in mg/L	Chl°

➤ Part B : chlorine residual measurement (break-point test)

- 5- Fill in the following table with the results obtained during the measurements carried out: (the 15 chl° bleach used is 100 times diluted (solution "S" i.e. 0.48 g/L).

Samples \rightarrow (beker N°)	①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
Concentration "C" of active or added chlorine (mg/l)	0.5	0.75	1	1.5	1.75	2	3	4	5	6
Volume (V'_p) de Cl_2 ajouté à 100 ml d'eau à traiter	0.105	0.157	0.210	0.315	0.368	0.420	0.630	0.841	1.051	1.261
$V_{e(B)}$ (chlorine residual measurement) in ml										
$[Cl_2]_{résiduel}$ in mg/L (Total residual chlorine concentration)										
Samples \rightarrow (beker N°)	⑪	⑫	⑬	⑭	⑮	⑯	⑰	⑱	⑲	⑳

Concentration "C" of active or added chlorine (mg/l)	7	8	9	10	11	12	13	14	15	20
Volume (V'p) de Cl ₂ ajouté à 100 ml d'eau à traité	1.472	1.682	1.892	2.103	2.313	2.523	2.734	2.944	3.154	4.206
V _{e(B)} (chlorine residual measurement) in ml										
[Cl ₂] _{résiduel} in mg/L (Total residual chlorine concentration)										

2-Draw the graph: (either with **Regressi**® software or on millimetric paper)

$$[Cl_2]_{\text{Total residual}} \text{ (mg/L)} = f([Cl_2]_{\text{Active or Added in mg/L}})$$

3-From the graph, determine the coordinates of the breakpoint.

4-Calculate the amount of chlorine consumed (mg/L) at the breakpoint.

Expression of results:

$$[Cl_2]_{\text{consommé}} \text{ (mg / L)} = [Cl_2]_{\text{ajouter}} \text{ (mg / L)} - [Cl_2]_{\text{résiduel}} \text{ (mg / L)}$$

5-What is the difference between "sterilization" and "disinfection"?

6-Conclude (compare the value of chlorine actually consumed with that indicated in the theory 7.6 mg/L)

APPENDIX

The volumes to be taken for a 12Chl° bleach (100 times diluted, solution "S" i.e. 0.38 g/L).

Samples → (bekersN°)	①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
Volume(V'p)of Cl ₂ added at100 ml treated water	0.131	0.197	0.263	0.394	0.460	0.526	0.789	1.052	1.315	1.579
Samples → (bekersN°)	⑪	⑫	⑬	⑭	⑮	⑯	⑰	⑱	⑲	⑳
Volume(V'p)of Cl ₂ added at100 ml treated water	1.842	2.105	2.368	2.631	2.894	3.158	3.421	3.684	3.947	5.263

The volumes to be taken for 16Chl° bleach (100 times diluted, solution "S" i.e. 0.51 g/L).

Samples → (bekersN°)	①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
Volume(V'p)of Cl ₂ added at100 ml treated water	0.100	0.150	0.200	0.295	0.345	0.400	0.600	0.788	0.986	1.183
Samples → (bekersN°)	⑪	⑫	⑬	⑭	⑮	⑯	⑰	⑱	⑲	⑳
Volume(V'p)of Cl ₂ added at100 ml treated water	1.380	1.577	1.775	1.971	2.170	2.366	2.563	2.760	3.000	3.943

References

- *Jean Rodier, Bernard Legube, Nicole Merlet, L'analyse de l'eau. Eaux naturelles, eaux résiduaires, eau de mer, édition Dunod, Septembre 2016 - 10ème édition.*
- Masschelein W.J. , Processus unitaires du traitement des eaux , Ed CEBEDOC 1996 , 493p.
- Anonyme, Mémento technique de l'eau (Tome 1 et 2), Ed. Degremont-Suez, 10 édition, 2005, 1904 p.
- Raymond Desjardins, Le Traitement des Eaux, Ed. Ecole Polytechnique de Montréal, 1997, 303 p.
- Alain Maurel, Dessalement de l'eau de mer et des eaux saumâtres, Et autres procédés non conventionnels d'approvisionnement en eau douce ED Tec et Doc - Lavoisier, 2001, 226p
- Mohand Said OUALI, Procédés unitaires biologiques et traitement des eaux, ED OPU, 156p
- Marcel Doré, Chimie des Oxydants et traitement des eaux, Ed TEC et Doc, 1998, 505p
- Claud, Cardot, Les traitements des eaux , procédés physico-chimiques et biologiques cours et problèmes résolus, Ed Ellipses, 2002,252p